

WET DUST CLEANER RESEARCH OF HYDRODYNAMIC REGIME

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ABSTRACT	KEYWORDS
The article describes a device that generates a contact element current that purifies dusty gas in a wet manner. Theoretical research work on determining the total hydraulic resistance is presented. A calculation scheme of the device for theoretical calculation work is developed. The equations of hydraulic resistance affecting the fluid flow according to the nozzle hole and diameter of the calculation scheme are presented.	Wet method, spark flow, spark generator, contact element, dusty gas, toxic gas, air flow, gas flow, gas velocity, cyclone, dusty air, fan, cone mesh, disperser, biological microscope

Introduction

For the correct implementation of technological processes in manufacturing enterprises, industrial dusty gases must be cleaned of dust. Mixers, dispersers, and most mass transfer devices cannot function properly without effective gas and dust cleaning schemes [1,2,3]. Today The following methods are used to clean dusty gas mixtures.

Centrifugal force sedimentation; gravity sedimentation; sedimentation in electric and other force fields; filtration; wet gas purification.

When analyzing these dust and gas cleaning methods, wet cleaning is the most effective. Currently, there is a trend towards widespread use of this method in industry, and many scientific research works are being conducted in this area [4,5].

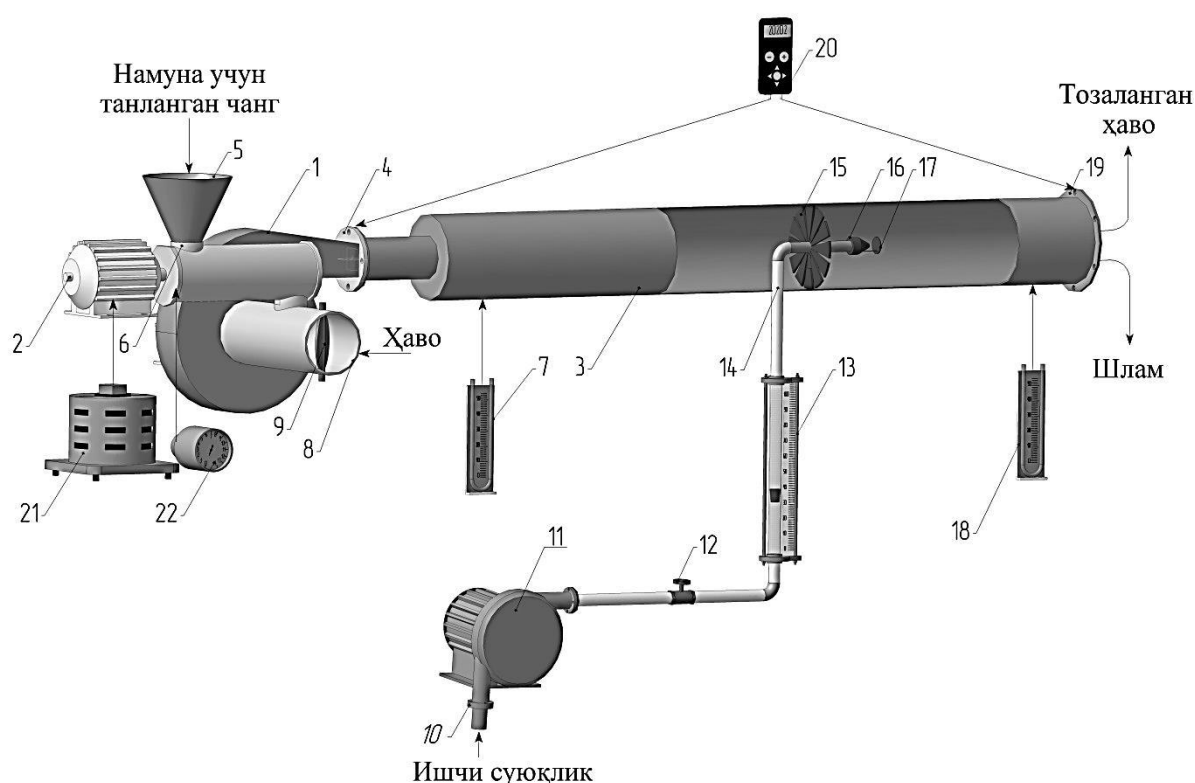
For example, when using this type of device, the dust flow is in contact with the liquid in the form of drops or films. Due to the hydrophilic property, the dust adheres to the surface of the liquid and is removed from the device with it. In addition, it can capture very small particles (up to 0.1 μm) and has a high cleaning capacity (up to 99%). However, the formation of liquid sludge when using this

type of device and the additional energy consumption for its re-cleaning require research and development in this area.

Dusty gas cleaning devices using the wet method are aimed at increasing the efficiency of dust and gas cleaning with low fluid consumption. This, in turn, allows for reduced energy consumption.

Based on the above, dusty gases Based on numerous research studies conducted on the designs of wet cleaning and neutralization devices and an analysis of their advantages and disadvantages, a structural scheme of a wet dust cleaning device has been developed. [6]Figure 1.

Developed device To study the effect of hydraulic resistance on cleaning efficiency and energy consumption, its hydrodynamics were theoretically studied. Figure 2 shows the calculation scheme of the device.



- 1- fan ; 2-electric motor; 3- metal pipe ; 4,10,19 - flanges; 5-powder loading device; 6-supply; 7,18 - Prandl tube; 8-powder gas inlet pipe; 9- slide ; 11-pump; 12- valve; 13- r a t o meter; 14-water delivery pipe; 15-gas flow regulator contact element; (swivel) 16- liquid nozzle; 17- water deflector; 20- anemometer; 21- LATR; 22 - tachometer.

Figure 1. General view of the device.

The device acting on the fluid can be written as follows

$$\Delta P_{\text{сую}} = P_{\kappa} + P_{\text{ш}} , \text{ Pa} \quad (1)$$

in this: P_{κ} – is the geometric pressure inside the pipe through which the liquid flows, and is determined by the following equation.

$$P_{\kappa} = \rho g H , \text{ Pa} \quad (2)$$

in this: ρ – density of the liquid, kg/m^3 ; g – acceleration of gravity, m/s^2 ; H – liquid level height, m;

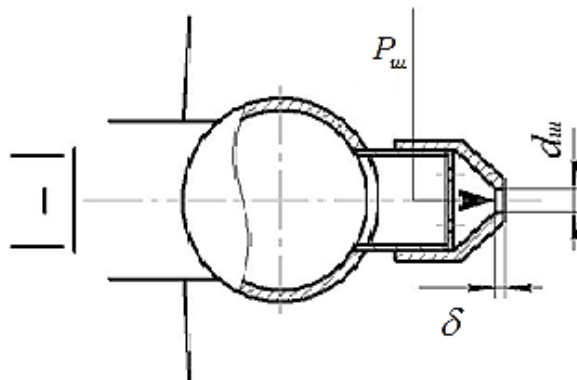
P_{uu} – is the pressure loss when the fluid flows through the hole, which is determined by the Darcy – Weisbach equation[7].

$$P_{uu} = \zeta_{uu} \frac{\rho_c \cdot g_c^2}{2}, \text{Pa} \quad (3)$$

in this: g_c – the velocity of the liquid flowing out of the hole, m/s; ζ_{uu} – the coefficient of resistance to the flow of the liquid through the nozzle hole, which depends on the thickness of the nozzle hole δ and the hole diameter d_{sh} .

In this case, to determine the velocity of the fluid flowing through the nozzle of the device, P_k we apply Bernoulli's equation, assuming that the pressure in the pipe and the pressure at the nozzle P_{uu} are equal. In this case, equation (4) can be written as follows:

$$\rho_c g H = \zeta_{uu} \frac{\rho_c \cdot g_c^2}{2}, \text{Pa} \quad (4)$$



1. Figure 2. The coefficient of resistance of the Shtüsser calculation scheme

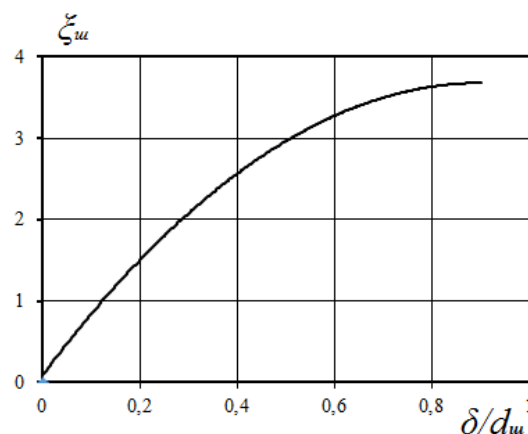


Figure 1.3. Dependence of P_{sh} on δ and d_k .

From the resulting equation (4), we determine the fluid velocity, m/s:

$$g_c = \sqrt{\frac{2(\rho_c g H)}{\rho_c \zeta}} = \sqrt{\frac{2gH}{\zeta}}, \text{m/s} \quad (5)$$

From equation (5), it is possible to determine the flow rate of fluid flowing through the device's nozzle hole.

$$Q_c = 3600 \pi R^2 g_c, \text{m}^3/\text{hour} \quad (6)$$

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